Supporting Information for

# A Flexible Tribotronic Artificial Synapse with Bioinspired Neurosensory Behavior

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## **Supplementary Figures and Tables**



Fig. S1 Impedance analysis of the ion-gel dielectric film. (a) Typical MIM structure diagram of the ion-gel dielectric film. (b) The functional relationship between the capacitance of the ion-gel dielectric film and the frequency of applied AC. (c) The functional relationship between the phase angle of the ion-gel dielectric film and the frequency of applied AC. (d) Nyquist plot of the ion-gel dielectric film



**Fig. S2** Characterization of the P3HT-NF/PDMS semiconductor. (**a**) Optical image after complete dissolution of P3HT. (**b**) Optical image of the P3HT-NF/PDMS semiconductor solution. (**c**) The AFM morphology of the P3HT-NF/PDMS semiconductor film



**Fig. S3** The bending process diagram and electrical characteristics of the OTFT. (**a**) Schematic illustration of the OTFT in tensile and compressive strain states, respectively. (**b**) Double-sweep transfer characteristics of the OTFT under different bending radius in tensile strain states. (**c**) Double-sweep transfer characteristics of the OTFT under different bending radius in compressive strain states. (**d**) Double-sweep transfer characteristics of the OTFT under different  $V_d$ . (**e**) Double-sweep transfer characteristics of the OTFT after different number of tensile strain cycles with a bending radius of 20 mm. (**f**) Double-sweep transfer characteristics of the OTFT after different number of compressive strain cycles with a bending radius of 20 mm. (**g**) The mobility of the OTFT after different number of tensile and compressive strain cycles with a bending radius of 20 mm.



**Fig. S4** The fitting of the EPSC decay behavior with stretched-exponential decay model. (**a-f**) The fitting of the EPSC decay behavior with stretched-exponential decay model under single mechanical stimuli with different duration time (0.1 s, 0.3 s, 0.6 s, 1.0 s, 1.6 s and 2.5 s)



**Fig. S5** The effect of different bending radius on EPSC peak value of the TAS under single mechanical stimuli with different duration time. (a) The effect of different bending radius in tensile strain states on EPSC peak value of the TAS under single mechanical stimuli with different duration time. (b) The effect of different bending radius in compressive strain states on EPSC peak value of the TAS under single mechanical stimuli with different duration time.



**Fig. S6** The effect of different bending radius on PPF index of the TAS under paired mechanical stimuli with different interval time. (**a**) The effect of different bending radius in tensile strain states on PPF index of the TAS under paired mechanical stimuli with different interval time. (**b**) The effect of different bending radius in compressive strain states on PPF index of the TAS under paired mechanical stimuli with different interval time. (**b**) The effect of different bending radius in compressive strain states on PPF index of the TAS under paired mechanical stimuli with different interval time.



**Fig. S7** EPSC and PPF index response of the TAS under different bending radius in tensile strain states. (**a**), (**c**), (**e**), (**g**) and (**i**) The EPSC response of the TAS under different bending radius (20, 40, 60, 80 and 100 mm) in tensile strain states, respectively. (**b**), (**d**), (**f**), (**h**) and (**j**) The PPF index response of the TAS under different bending radius (20, 40, 60, 80 and 100 mm) in tensile strain states.



**Fig. S8** The EPSC and PPF index response of the TAS under different bending radius in compressive strain states. (**a**), (**c**), (**g**) and (**i**) The EPSC response of the TAS under different bending radius (20, 40, 60, 80 and 100 mm) in compressive strain states, respectively. (**b**), (**d**), (**f**), (**h**) and (**j**) The PPF index response of the TAS under different bending radius (20, 40, 60, 80 and 100 mm) in compressive strain states, respectively. (**b**), (**d**), 80 and 100 mm) in compressive strain states, respectively.



**Fig. S9** The effect of different bending radius on the output characteristics of the TAS under multiple mechanical stimuli with a duration time of 0.1 s. (a) The effect of different bending radius in tensile strain states on the EPSC peak value of the TAS under multiple mechanical stimuli with a duration time of 0.1 s. (b) The effect of different bending radius in compressive strain states on the EPSC peak value of the TAS under multiple mechanical stimuli with a duration time of 0.1 s. (c) The effect of the different bending radius in tensile strain states on the EPSC gain of the TAS (EPSC gain is defined as  $A_n/A_1$ ) under multiple continuous mechanical stimuli with a duration time of 0.1 s. (d) The effect of the different bending radius in tensile strain states on the EPSC gain of the EPSC gain of the TAS (EPSC gain of the TAS (EPSC gain is defined as  $A_n/A_1$ ) under multiple continuous mechanical stimuli with a duration time of 0.1 s. (d) The effect of the different bending radius in tensile strain states on the EPSC gain of the TAS (EPSC gain is defined as  $A_n/A_1$ ) under multiple continuous mechanical stimuli with a duration time of 0.1 s. (d) The effect of the different bending radius in compressive strain states on the EPSC gain of the TAS (EPSC gain is defined as  $A_n/A_1$ ) under multiple continuous mechanical stimuli with a duration time of 0.1 s.



**Fig. S10** EPSC and PPF index response of the TAS after tensile strain cycles with bending radius of 20 mm. (**a**), (**c**), (**e**), (**g**) and (**i**) The EPSC response of the TAS after different tensile strain cycles (200, 400, 600, 800 and 1000) with bending radius of 20 mm, respectively. (**b**), (**d**), (**f**), (**h**) and (**j**) The EPSC response of the TAS after different tensile strain cycles (200, 400, 600, 800 and 1000) with bending radius of 20 mm, respectively. (**b**), (**d**), (**f**), (**h**) and (**j**) The EPSC response of the TAS after different tensile strain cycles (200, 400, 600, 800 and 1000) with bending radius of 20 mm



**Fig. S11.** The EPSC and PPF index responses of the TAS after compressive strain cycles with bending radius of 20 mm. (**a**), (**c**), (**e**), (**g**) and (**i**) The EPSC response of the TAS after different compressive strain cycles (200, 400, 600, 800 and 1000) with bending radius of 20 mm, respectively. (**b**), (**d**), (**f**), (**h**) and (**j**) The EPSC response of the TAS after different compressive strain cycles (200, 400, 600, and 1000) with bending radius of 20 mm,



**Fig. S12** The effect of the number of tensile and compressive strain cycles with a bending radius of 20 mm on the EPSC gain of the TAS (EPSC gain is defined as  $A_n/A_1$ ) under multiple continuous mechanical stimuli with a duration time of 0.1 s. (a) The effect of the number of tensile strain cycles with a bending radius of 20 mm on the EPSC gain of the TAS under multiple continuous mechanical stimuli with a duration time of 0.1 s. (b) The effect of the number of compressive strain cycles with a bending radius of 20 mm on the EPSC gain of the TAS under multiple continuous mechanical stimuli with a duration time of 0.1 s. (b) The effect of the number of compressive strain cycles with a bending radius of 20 mm on the EPSC gain of the TAS under multiple continuous mechanical stimuli with a duration time of 0.1 s.

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Activation modes	Substrate	Electrodes	Active layer	Dielectric layer	Stimuli signal	EPSC Decay time	PPF A <sup>2</sup> /A <sup>1</sup>	SM to LTM Retention time	Refs.
External power	ITO glass	IZO	IZO	Chitosan	Electrical pulse	N/A	~1.36	8 s	[S1]
Piezoelectric	PET	Cr/Au	Graphene	PEGDA+HOMPP EMIM-TFSI	Force	3.24 s	~1.4		[S2]
Triboelectric	Si	Cr/Au	$MoS_2$	PSSH	Force	N/A	1.16		[ <b>S</b> 3]
	Si	Cr/Au	$MoS_2$	PEGDA+HOMPP EMIM-TFSI	Force	75 ms	~1.4	~10 s	[S4]
	PET	Ti/Au	P3HT- NF/PDMS	PVDF-HFP +EMIM-TFSI	Force / Vibration	6.89 s	1.56	30 s	This work

# Table S1 The comparison of the reported artificial synapses in previous literature

### **Supplementary References**

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