

Supporting Information for

# Highly Thermoconductive, Strong Graphene-Based Composite Films by Eliminating Nanosheets Wrinkles

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## S1 Supporting Methods

### S1.1 Calculation of Herman's Order Parameter

Wide-angle X-ray scattering (WAXS) measurement was conducted on a Xenocs Xeuss 2.0 System by using an incident Cu-K $\alpha$  X-ray beam that is parallel to film plane. X-ray wavelength, spot size, and distance between specimen and detector were 0.1542 nm,  $172 \times 172 \mu\text{m}^2$ , and 88 mm, respectively. Samples were square slices with a side length of 10 mm. Scattering patterns were collected by a Pilatus 300 k detector. Orientation factor ( $f$ ) was calculated to describe orientation degree of GNS. Its value ranges from 0 to 1, where the former corresponds to an isotropic structure and the latter corresponds to a perfect orientation structure along the director. A Maier-Saupe distribution function was used to fit the azimuthal profile.

$$I = I_0 + A \exp[\omega \cos^2 (\varphi - \varphi_0)]$$

where  $I_0$  is the free baseline,  $\varphi$  is the azimuthal angle,  $\varphi_0$  is the azimuth at the position of maximal intensity, and  $\omega$  is a parameter that determines the width of the distribution. After the fitting, parameter  $\omega$  was obtained, and the orientation factor  $f$  can be determined using the following formula

$$f = \frac{\int_{-1}^1 P_2(\cos \varphi) \exp(\omega \cos^2 \varphi) d(\cos \varphi)}{\int_{-1}^1 \exp(\omega \cos^2 \varphi) d(\cos \varphi)}$$

where the function  $P_2(\cos \varphi)$  is the second-order Legendre polynomial of  $\cos \varphi$  and often referred to as the Herman's order parameter function:

$$P_2(\cos \varphi) = \frac{1}{2} (3 \cos^2 \varphi - 1)$$

## S1.2 Phonon Density of States (PDOS) Analysis

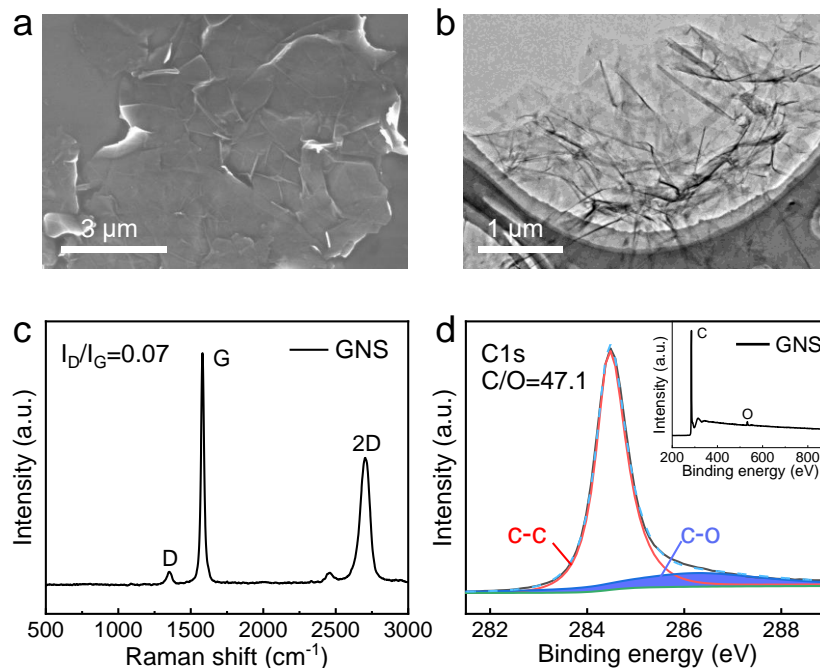
The first-principles calculations are performed using the Vienna Ab initio Simulation Package (VASP) based on the density functional theory (DFT). The generalized gradient approximation (GGA) of the Perdew-Burke-Ernzerhof (PBE) form is used for the exchange-correlation functional. The second-order harmonic interatomic force constants (IFCs) are calculated through the Hessian matrix using the density functional perturbation theory (DFPT). The phonon frequencies are then obtained using the PHONOPY package. To calculate the IFCs, a  $4 \times 4 \times 1$  supercell with a  $3 \times 3 \times 1$  q-point mesh is employed for graphene, and a  $1 \times 1 \times 2$  supercell with a  $1 \times 1 \times 3$  q-point mesh is employed for ANF.

For graphene, the kinetic energy cutoff is set to 500 eV and a  $12 \times 12 \times 1$  Monkhorst-Pack k-point mesh is adopted. The structure is fully relaxed until the force on each atom is less than  $10^{-4}$  eV/Å. The calculated lattice constant of graphene is 2.46 Å. For the aramid nanofiber (ANF), the lattice constants of the primitive cell for the p-phenylene terephthalamide (PPTA) are set to  $a=15.74$  Å,  $b=15.54$  Å, and  $c=12.9$  Å. Then the one-dimensional ANF is constructed by a  $2 \times 3 \times 1$  supercell and the chain orientation is the z-axis. A vacuum space of 15 Å is used to avoid interaction between two adjacent supercells. The kinetic energy cutoff is set to 450 eV and a  $1 \times 1 \times 3$   $\Gamma$ -centered k-point mesh is adopted. The structure is fully relaxed until the force convergence threshold of 0.02 eV/Å is satisfied.

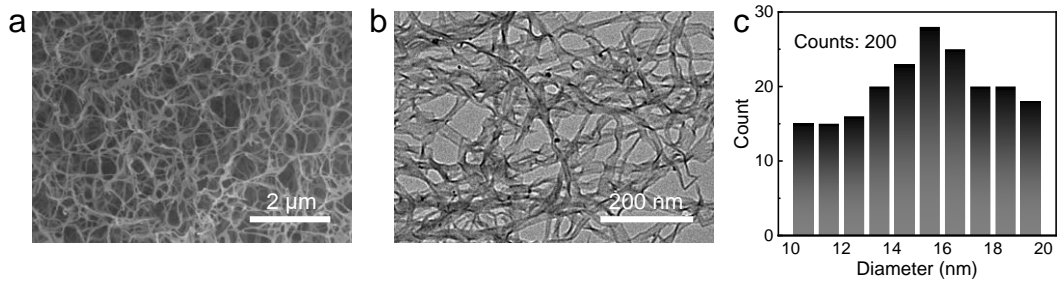
## S1.3 Finite Element Mode

The heat transfer processes of spontaneously dried and constrained dried GNS/ANF-60 wt% films are modeled in COMSOL multiphysics software, which used a transient simulation model. Herein, the in-plane and out-of-plane thermal conductivity of GNS/ANF-0 % films are set to be  $81.0 \text{ W m}^{-1} \text{ K}^{-1}$  and  $0.41 \text{ W m}^{-1} \text{ K}^{-1}$ . The in-plane and out-of-plane thermal conductivity of GNS/ANF-15% films are set to be  $146.0 \text{ W m}^{-1} \text{ K}^{-1}$  and  $0.79 \text{ W m}^{-1} \text{ K}^{-1}$ . The ambient temperature is 25 °C.

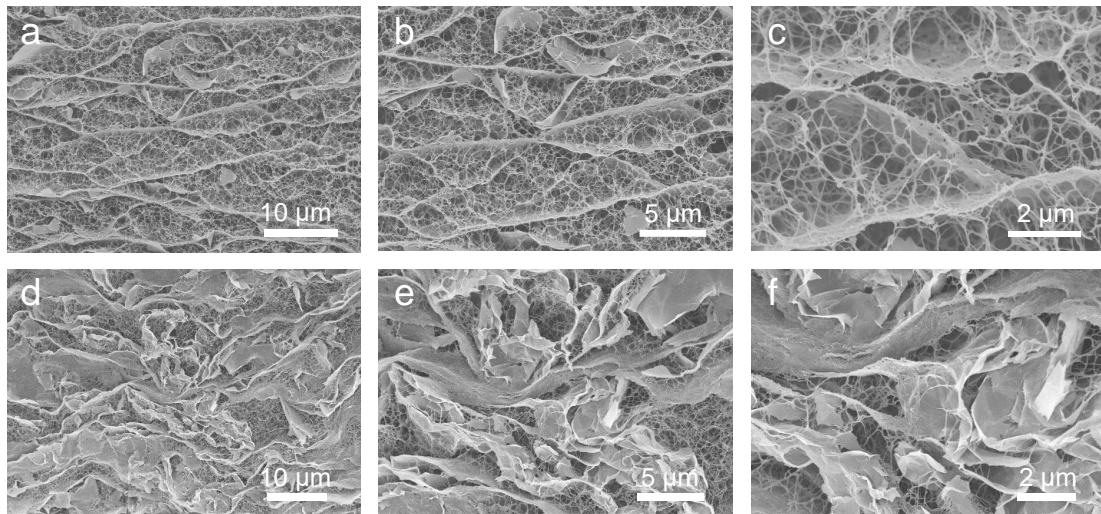
## S2 Supplementary Figures



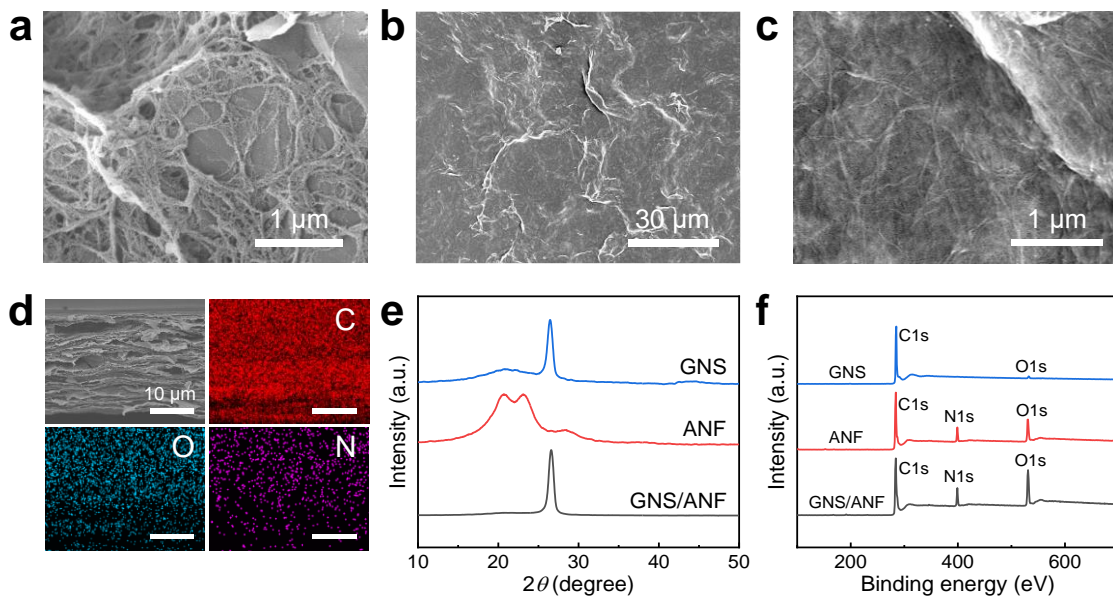
**Fig. S1** Characterization of graphene nanosheets. **a** SEM and **b** TEM images of graphene nanosheets. **c** Raman spectra and **d** XPS spectra of graphene nanosheets



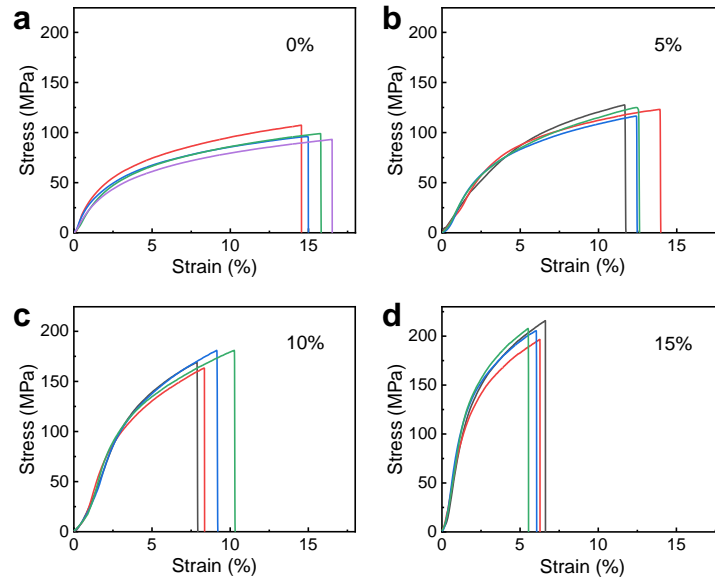
**Fig. S2** Characterization of aramid nanofiber. **a** SEM and **b** TEM images of ANF. **c** Statistical data showing the diameter of ANF



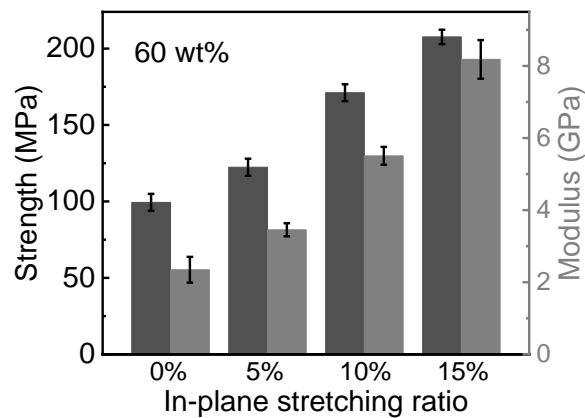
**Fig. S3** SEM images for GNS/ANF composite aerogel with different in-plane stretching ratio. **a-c** 15%, **d-f** 0%



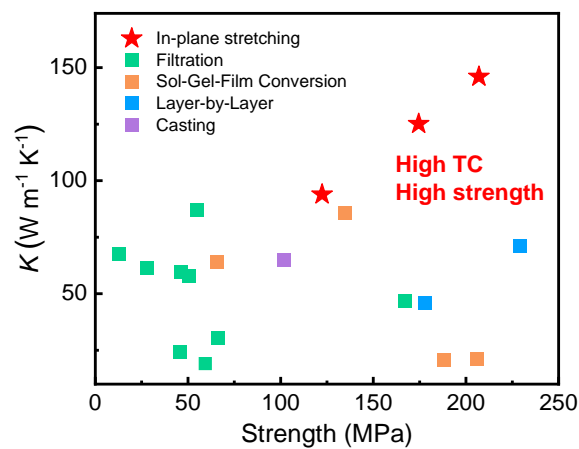
**Fig. S4** Characterization of GNS/ANF composite films. **a** SEM image of aerogel. **b, c** Surface SEM image. **d** Cross-sectional SEM images along with elemental mapping images. **e** XRD patterns. **f** XPS spectra



**Fig. S5** Tensile stress-strain curves of GNS/ANF-60 wt% films by different in-plane stretching ratio. **a** 0%, **b** 5%, **c** 10%, and **d** 15%

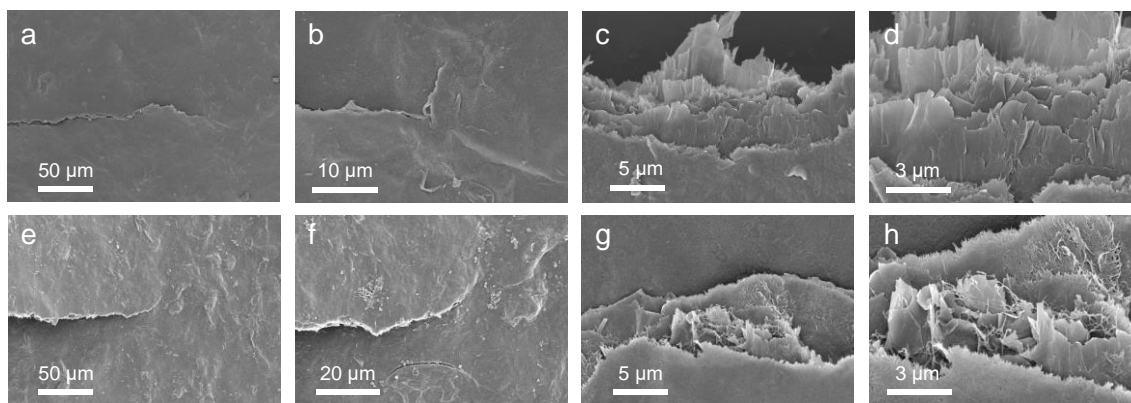


**Fig. S6** Strength and modulus of GNS/ANF-60 wt% films by different in-plane stretching ratio

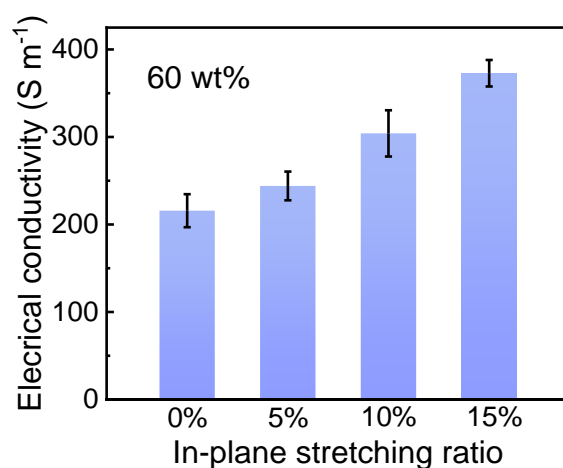


**Fig. S7** Comparison of thermal conductivity and tensile strength of composite films assembled by in-plane stretching and previously reported spontaneous assembly thermal management materials

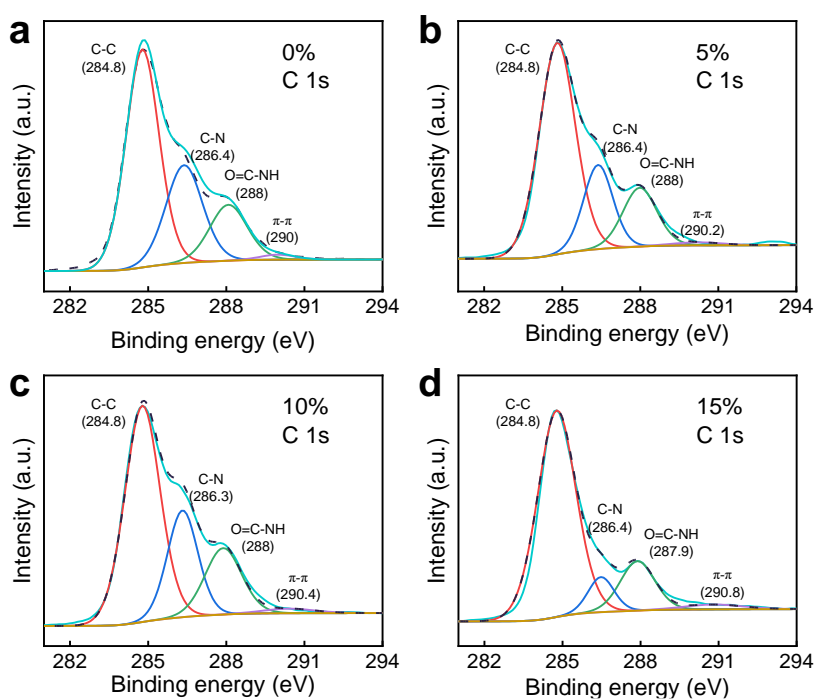




**Fig. S8** Fracture behavior of GNS/ANF-60 wt% films by different in-plane stretching ratio. **a-d** 15%, **e-h** 0%



**Fig. S9** Electrical conductivity of GNS/ANF-60 wt% films by different in-plane stretching ratio



**Fig. S10** High-resolution XPS spectra of C 1s for GNS/ANF-60 wt% films by different in-plane stretching ratio. **a** 0%, **b** 5%, **c** 10%, **d** 15%

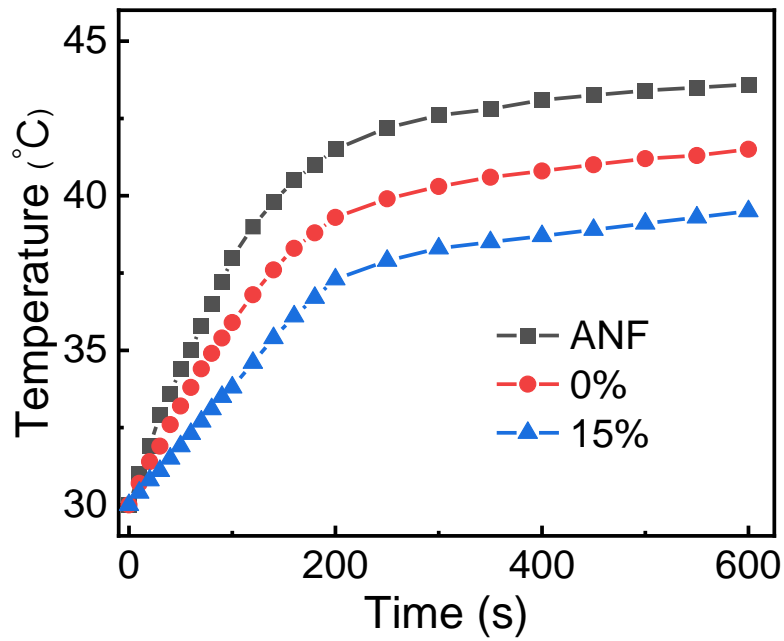


Fig. S11 Temperature evolution curves of smartphones with working time

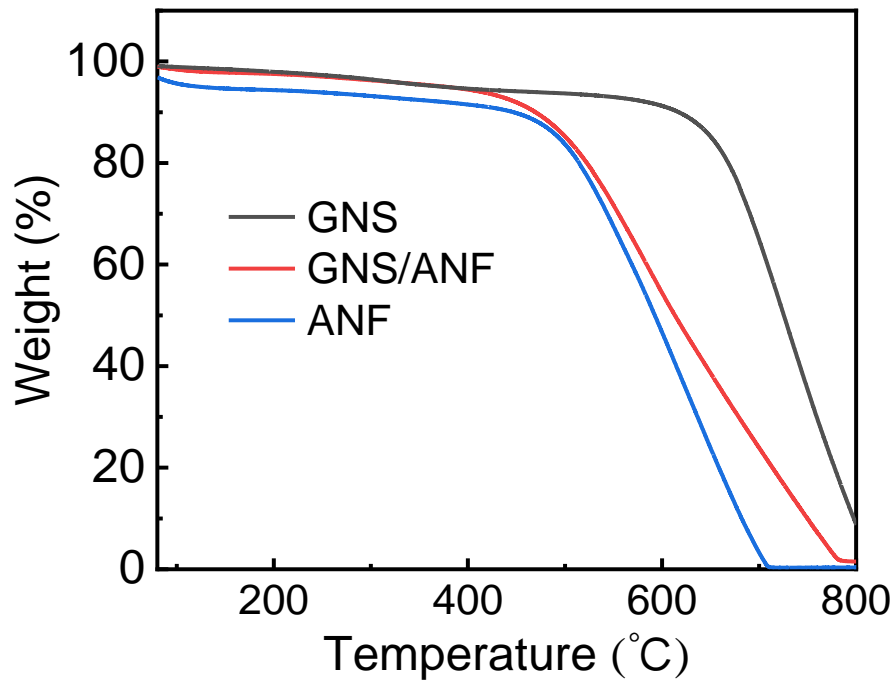


Fig. S12 TGA curves of GNS, GNS/ANF-60 wt% and ANF

## Supplementary Tables

**Table S1** Fillers, nanosheets conformation, matrix, in-plane thermal conductivity ( $K$ ) and tensile strength ( $\sigma$ ) of GNS/ANF composite films with eliminated nanosheets wrinkles were compared with those of thermally conductive composite films with nanosheets wrinkles

Fillers	Nanosheets conformation	Matrix	In-plane $K$ ( $\text{W m}^{-1} \text{K}^{-1}$ )	$\sigma$ (MPa)	Refs.
73.3 wt% GF	wrinkles	PVA	21.6	84.4	[S1]
93 wt% GF	wrinkles	PVA	61.3	28	[S1]
40 wt% GF	wrinkles	ANF	48.2	188	[S2]
70 wt% CPGO	wrinkles	CNF	12.8	33.5	[S3]
30 wt% RGO	wrinkles	CNF	6.2	90	[S4]
32.8 wt% GNS	wrinkles	PVA	45.8	177.8	[S5]
55.7 wt% GNS	wrinkles	PVA	71.2	229.4	[S5]
61 wt% GNS	wrinkles	PVA	82.4	259	[S5]
10 wt% GNS	wrinkles	PVA	13.8	84	[S6]
50 wt% GNS	wrinkles	PI	65	102	[S7]
80 wt% GNS	wrinkles	ANF	87.1	55	[S8]
50 wt% GNS	wrinkles	ANF	76.9	145.1	[S9]
60 wt% GNS	wrinkles	ANF	85.6	134.5	[S9]
60 wt% GNS	wrinkles	ANF	85.3	266	[S10]
75 wt% GNS	wrinkles	CNF	58	50.7	[S11]
61 wt% GNS	wrinkles	CNF	134.1	51.9	[S12]
75 wt% GNS	wrinkles	CNF	59.5	46.4	[S13]
40 wt% GNS	wrinkles	PBONF	87.2	188.9	[S14]
50 wt% GNS	wrinkles	PBONF	98.7	194.7	[S14]
30 wt% MXene@Ag	wrinkles	CNF	22.4	71.4	[S15]
60 wt% MXene	wrinkles	CNF	14.9	114.4	[S16]
<b>60 wt% GNS</b>	<b>Eliminated wrinkles</b>	<b>ANF</b>	<b>146</b>	<b>207</b>	<b>This work</b>

GF: Fluorinated graphene; CPGO: Casein phosphopeptide-biofunctionalized graphene oxide nanoplatelets; RGO: Reduced graphene oxide; GNS: Graphene nanosheets; PVA: Poly(vinyl alcohol); PI: Polyimide; ANF: Aramid nanofiber; CNF: Cellulose nanofiber; PBONF: poly(p-phenylene benzobisoxazole) nanofiber

**Table S2** Thermal conductivity of constrained dried GNS/ANF-60 wt% films by different in-plane stretching ratio at 25 °C

In-plane stretching ratio	Thermal conductivity ( $\text{W m}^{-1} \text{K}^{-1}$ )	
	In-plane	Out-of-plane
0%	$81.0 \pm 3.0$	$0.41 \pm 0.02$
5%	$93.9 \pm 3.4$	$0.46 \pm 0.02$
10%	$125.1 \pm 3.1$	$0.58 \pm 0.03$
15%	$146.0 \pm 3.5$	$0.79 \pm 0.05$

**Table S3** Strength at break ( $\sigma$ ), Young's modulus ( $E$ ), strain at break ( $\varepsilon$ ) and toughness ( $U$ ) of GNS/ANF-60 wt% films by different in-plane stretching ratio

in-plane stretching ratio	$\sigma$ (MPa)	$E$ (GPa)	$\varepsilon$ (%)	$U$ (MJ m <sup>-3</sup> )
0%	99.4 ± 5.5	2.3 ± 0.3	15.4 ± 0.9	11.2 ± 0.3
5%	122.4 ± 5.6	3.5 ± 0.2	12.6 ± 0.7	10.8 ± 0.6
10%	174.5 ± 5.9	5.5 ± 0.2	9.1 ± 0.5	9.2 ± 0.3
15%	207.0 ± 4.7	8.2 ± 0.5	6.3 ± 0.3	9.1 ± 0.6

**Table S4** Assembly, fillers, matrix, in-plane thermal conductivity ( $K$ ) and tensile strength ( $\sigma$ ) of GNS/ANF composite films prepared by in-plane stretching constrained dried strategy were compared with those of thermally conductive composite films prepared by spontaneous dried strategies such as vacuum-assisted filtration, sol-gel-film conversion, layer-by-layer and casting

Assembly	Fillers	Matrix	In-plane $K$ (W m <sup>-1</sup> K <sup>-1</sup> )	$\sigma$ (MPa)	Refs.
VAF	93 wt% GF	PVA	61.3	28	[S1]
VAF	80 wt% GNS	ANF	87.2	55	[S8]
VAF	75 wt% GNS	CNF	58	50.7	[S11]
VAF	75 wt% GNS	CNF	59.5	46.4	[S13]
VAF	83 wt% BNNS	CNF	67.6	13	[S17]
VAF	30 wt% BNNS	ANF	46.7	167	[S18]
VAF	50 wt% BNNS	ANF	19.1	59.3	[S19]
VAF	70 wt% BNNS	CNF	30.3	66	[S20]
VAF	60 wt% BNNS	CNF	24.3	45.5	[S21]
Sol-Gel-Film Conversion	40 wt% GF	ANF	20.5	188	[S2]
Sol-Gel-Film Conversion	60 wt% GNS	ANF	85.6	134.5	[S9]
Sol-Gel-Film Conversion	50 wt% BNNS	ANF	64.1	65.6	[S22]
Sol-Gel-Film Conversion	10 wt% BNNS	PBONF	21.3	206	[S23]
Layer-by-Layer	55.7 wt% GNS	PVA	71.2	229.4	[S5]
Layer-by-Layer	32.8 wt% GNS	PVA	45.8	177.8	[S5]
Casting	50 wt% GNS	PI	65	102	[S7]
<b>In-plane stretching</b>	<b>60 wt% GNS</b>	<b>ANF</b>	<b>93.9</b>	<b>122.4</b>	<b>This work<sup>1</sup></b>
<b>In-plane stretching</b>	<b>60 wt% GNS</b>	<b>ANF</b>	<b>125.1</b>	<b>174.5</b>	<b>This work<sup>2</sup></b>
<b>In-plane stretching</b>	<b>60 wt% GNS</b>	<b>ANF</b>	<b>146</b>	<b>207</b>	<b>This work<sup>3</sup></b>

VAF: Vacuum-assisted filtration; This work1, this work2 and this work3: Constrained dried GNS/ANF-60 wt% films by in-plane stretching for (1) 5%, (2) 10%, and (3) 15%.

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