Supporting Information for

Designing Electronic Structures of Multiscale Helical Converters for Tailored Ultrabroad Electromagnetic Absorption

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S1 Experimental Section

L-phenylglycine, (CH3COO)2Mn·4H2O, and anhydrous methanol were purchased from Bide Pharmatech Co., Ltd. (Shanghai, China). Palmitoyl chloride, NaOH, acetone, formalin aqueous solution (37 wt%), petroleum ether, and 3-aminophenol (3-AP) were purchased form Aladdin Biochemical Technology Co., Ltd. (Shanghai, China). All chemicals were used without further purification.

S1.1 Synthesis of HM, SHM, and LHM

A solution containing 0.09 mmol of the antisense strand (AS), 1.83 mmol of 3-AP, 0.09 mmol of (CH3COO)2Mn·4H2O were added into 8 mL of anhydrous methanol, and heated to 60 °C. Subsequently, 62 mL of deionized water was added, followed by continuous stirring for 20 min, and the product was denoted as HM. Following a similar synthesis process as for HM, the amount of 3-AP was adjusted 0.91 mmol, and this product was named as SHM; while the amount of (CH3COO)2Mn·4H2O was changed to 0.45 mmol, which was denoted as LHM.

S1.2 Synthesis of 3-APFD and HC-8

3-AP (1.83 mmol) was completely dissolved in anhydrous methanol (8 mL) at 60 °C. Subsequently, deionized water (62 mL) was added to the above solution. After continuous stirring for 20 minutes, 200 μ L formalin aqueous solution (37 wt%) was added to induce polycondensation reaction, continuing for 2 h. The precursors were gathered through vacuum filtration and dried for 12 h, subsequently, were annealed under nitrogen atmosphere for 2 h at 800 °C at a rate of 2 °C/min, denoted as 3-APFD. Following a similar synthesis process as for 3-APFD, the AS (0.09 mmol) was added, which was named as HC-8.

S1.3 Characterization

¹H-Nuclear magnetic resonance $(^1H\text{-}NMR)$ spectra were recorded on a Bruker Avance III HD 500 MHz NMR spectrometer. The functional groups were detected by Fourier transform infrared spectroscopy (FT-IR; Bio-Rad FTS-40). The gradient mematerial, radar cross section (RCS) were simulated using computer simulation technology (CST Studio Suite 2022).

S1.4 Electromagnetic (EM) Measurements

The samples and paraffin were mixed in a certain proportion (the samples account for 30 wt%), and the coaxial ring with an inner diameter of 3.04 mm and an outer diameter of 7 mm was processed by the mold. As an electromagnetic wave absorption (EMWA) material, reflection loss (*RL*) and attenuation constant (*α*) are the important evaluation indexes. According to transmission line theory, *RL* and *α* can be calculated by the following formula [S1-S3]:

$$
Z_{in} = \sqrt{\frac{\mu_r}{\varepsilon_r}} \tanh[j(2\pi f d/c)\sqrt{\mu_r \varepsilon_r}]
$$
 (Eq. S1)

$$
RL = 20log|(Z_{in} - 1)/(Z_{in} + 1)|
$$
 (Eq. S2)

$$
\alpha = \frac{\sqrt{2}\pi f}{c} \sqrt{(\mu''\varepsilon'' - \mu'\varepsilon') + \sqrt{(\mu'\varepsilon'' + \mu''\varepsilon')^2 + (\mu''\varepsilon'' - \mu'\varepsilon')^2}}
$$
(Eq. S3)

Where *Zin* is the normalized input impedance of EMWA materials, *Z⁰* is the free space impedance; ε_r and μ_r represent complex permittivity and complex permeability, respectively; *d* is the thickness of the EMWA materials; *f* is the frequency of electromagnetic waves (EMWs). The Debye relaxation formula is an important means of studying polarization effect as follows [S4-S6]:

$$
(\varepsilon' - \frac{\varepsilon_s + \varepsilon_\infty}{2})^2 + (\varepsilon'')^2 = (\frac{\varepsilon_s - \varepsilon_\infty}{2})^2
$$
 (Eq. S4)

$$
\varepsilon' = \varepsilon_{\infty} + \frac{\varepsilon_s - \varepsilon_{\infty}}{1 + \omega^2 \tau^2}
$$
 (Eq. S5)

$$
\varepsilon^{\prime\prime} = \frac{\varepsilon_s - \varepsilon_\infty}{1 + \omega^2 \tau^2} \omega \tau + \frac{\sigma}{\omega \varepsilon_0} = \varepsilon_p^{\prime\prime} + \varepsilon_c^{\prime\prime}
$$
 (Eq. S6)

Where ε_{∞} represents the relative dielectric permittivity at infinite frequency and $\varepsilon_{\rm s}$ is the static dielectric permittivity, ω is the angular frequency, τ is the relaxation time and σ is the electric conductivity.

According to basic laws of dielectric and magnetic physics, the absorbed incident EM energy (*E0*) can be divided into two parts and expressed as follows [S7-S9]:

$$
E_0 = E_S + E_D \tag{Eq. S7}
$$

where E_S and E_D represent the energy of storage part and conversion part, respectively.

 E_S is contributed by the real part of the permittivity and permeability, which can be explained as follows:

$$
E_S = \pi f \varepsilon' E_0^2 + \pi f \mu' H_0^2
$$
 (Eq. S8)

 E_D is contributed by the imaginary part of the permittivity and permeability, which

can be expressed as follows:

$$
E_D = \pi f \varepsilon^{\prime \prime} E_0^2 + \pi f \mu^{\prime \prime} H_0^2 \tag{Eq. S9}
$$

where E_0 and H_0 are the electric and magnetic field intensity amplitude of EMWs, respectively.

As the loss can be divided into polarization (ε_p''), conduction (ε_c''), and magnetic loss (μ'') :

$$
E_P = \pi f \varepsilon_p^{\prime\prime} E_0^2 \tag{Eq. S10}
$$

$$
E_C = \pi f \varepsilon_c^{\prime \prime} E_0^2 \tag{Eq. S11}
$$

$$
E_M = \pi f \mu^{\prime \prime} H_0^2 \tag{Eq. S12}
$$

where E_p , E_c and E_M represent conversion energy contributed by polarization loss, conduction loss and magnetic loss, respectively.

The transformation rate of converted EMWs derived from polarization (*RP*) and conduction (*RC*), and magnetic loss (*RM*) can be expressed as follows:

$$
R_P = \frac{E_P}{E_D} \tag{Eq. S13}
$$

$$
R_C = \frac{E_C}{E_D} \tag{Eq. S14}
$$

$$
R_M = \frac{E_M}{E_D} \tag{Eq. S15}
$$

S1.5 Graphite domain size calculations

Graphite domain size (L_a) , defects distance (L_a) , and defect density (n_a) can be expressed as follows [12, 13]:

$$
L_{\alpha}(nm) = (2.4 \times 10^{-10}) \times \lambda^4 \times (I_D/I_G)^{-1}
$$
 (Eq. S16)

$$
L_d(nm) = \sqrt{(1.85 \times 10^{-9}) \times \lambda^4 \times (I_D/I_G)^{-1}}
$$
 (Eq. S17)

$$
n_d(nm) = (1.85 \times 10^{22}) \times \lambda^{-4} \times (I_D/I_G)
$$
 (Eq. S18)

S1.6 Maximum effective absorption integration area (*MEAIA***)**

The *MEAIA* is used to characterize its practical application potential:

$$
(\int R L (\le -10 \, dB) df)(t)^{-1} \tag{Eq. S19}
$$

where *t* represents the thickness of the thickness.

S1.7 EM simulation in CST

A template of periodic structures with metamaterial-full structure workflow was chosen for simulation. Frequency domain solver was used in this simulation process, the solving frequency is set to 2-18 GHz. The excitation type set to plane wave excitation, and the incident direction of EMW was vertical to the model. The tetrahedral mesh type was used to mesh these models.

S1.8 Quarter-wavelength theory

The relation between the *RL*, thickness, and frequency can be obtained using the quarter-wavelength model. The simulated thickness (*tm*) of an absorber at 2–18 GHz is estimated as follows:

$$
t_m = nc/(4f_m\sqrt{|\mu_r||\varepsilon_r|})
$$
 (Eq. S20)

where t_m , *n*, and f_m denote the simulated thickness, the refractive index of the material, and the matched frequency, respectively.

S1.9 RCS Simulation

The actual far-field response of the material was simulated using CST Studio Suite 2022. The material was modeled as a two-layer square model with a metallic base plate and an absorber layer, where the size of the square was $200 \text{ mm} \times 200 \text{ mm}$, the thickness of the absorber layer was x mm (x corresponds to the thickness of *RLmin* for each set of samples), and the thickness of the bottom perfectly conducting layer (PEC) was set to 2.0 mm. The model was placed in the X-O-Y plane, and the EMWs were incident from the positive direction of Z-axis. Adjusting the incident angle θ (-90°-90°) of EMWs while keeping the polarization angle φ constant, the RCS value can be expressed by *S* (area of the model), λ (wavelength of the EMW), E_s (electric field strength) and E_i (incident wave) [S10, S11].

$$
RCS(dBm^2) = 10 \log \left(\left(\frac{4\pi S}{\lambda^2} \right) \left| \frac{E_s}{E_i} \right| \right)^2 \tag{Eq. S21}
$$

S2 Results and Discussion

S2.1 FESEM of the AS, AS/3-AP, and HM

Fig. S1 FESEM of **a** AS, **b** AS/3-AP, and **c** HM

S2.2 FESEM of the varied geometric configurations

Fig. S2 FESEM of **a** SMC-8, **b** SHMC-8, **c** HMC-8, **d** LHMC-8, **e** LMC-8 and **f** 3- APFD

S2.3 HRTEM of the HMC-8

Fig. S3 HRTEM image of HMC-8

S2.4. XPS of SHMC-8 and LHMC-8

Fig. S4 a Full XPS survey spectra of SHMC-8 and LHMC-8, **b** N content and Mn content of SHMC-8, HMC-8, and LHMC-8

S2.5 ¹H-NMR and FT-IR of AS, AS/3-AP, HM, SHM and LHM

To explore the chemical structure and coordination information of AS, AS/3-AP, HM, SHM and LHM, ¹H-NMR and FT-IR were performed (Figs. S4a-b). The ¹H-NMR spectra of AS was well-matched with the prediction of ChemDraw, implying the successful synthesis of AS. AS: 1 H-NMR (500 MHz, DMSO-d6): δ =8.55 (s, 1H; CONHCH), 7.70-7.00 (m, 5H; Ph), 5.37 (d, J = 7.3 Hz, 1H; NHCHCOOH), 2.18 (t, J $= 7.3$ Hz, 2H; CH₂CH₂CONH), 1.48 (t, J = 7.6 Hz, 2H; CH₂CH₂CONH), 1.37-1.12 (m, 24H; alkyl), 0.85 (t, $J = 6.7$ Hz, 3H; CH₃CH₂).

The FT-IR showed that the new peaks did not appear in the AS/3-AP compound, suggesting that 3-AP was adsorbed on the surface of AS by electrostatic interaction. However, the addition of Mn ions significantly changed the coordination pattern, the $C=O$ stretching vibration in carboxylate disappears at 1726 cm⁻¹ and the new asymmetric stretching vibration of carboxylates appears at 1588 cm^{-1} and 1568 cm^{-1} . Meanwhile, the amide I and amide II bands shifted to low wavenumbers, with a significant decrease in intensity. The transmittance of the peaks assigned as N-H stretching vibrations also decreased. This observation implied that Mn^{2+} coordinated with carboxyl and amide units. Further, an increase in the amount of Mn^{2+} did not change the characteristic peaks of the FT-IR spectrum, suggesting that the amount of Mn^{2+} was excessive relative to the AS amount at this time, which also proved that the optimal ratio of Mn²⁺ to AS was 1:1. AS, FT-IR (KBr): 3292 (s) cm⁻¹ (N-H, amide A), 1648 (vs) cm−1 (CO, amide I), 1535 (vs) cm−1 (N-H, amide II).

Fig. S5 a ¹H-NMR of AS. **b** FT-IR of AS/3-AP, HM, SHM, LHM

S2.6 EAB of varied geometric configurations

Fig. S6 EAB curves of **a** SMC-8, **b** SHMC-8, **c** LHMC-8, and **d** LMC-8

S2.7 Electromagnetic parameters of varied geometric configurations

Fig. S7 a-b EM parameters of SMC-8, SHMC-8, HMC-8, LHMC-8, and LMC-8

S2.8 3D Cole-Cole curves of varied geometric configurations

Fig. S8 3D Cole–Cole curves of **a** SMC-8, **b** SHMC-8, **c** HMC-8, **d** LHMC-8, and **e** LMC-8

S2.9 The impedance matching and the attenuation constant of varied geometric configurations

Fig. S9 a-e The impedance matching and **f** the attenuation constant of SMC-8, SHMC-8, HMC-8, LHMC-8, and LMC-8

S2.10 The electromagnetic characteristic of 3-APFD and HC-8

The *RLmin* of 3-APFD is only −5.13 dB at a thickness of 1.78 mm because of the absence of the helical structure, which results in poor impedance matching and attenuation constant (**Fig. S10**).

Fig. S10 a 3D *RL* curve, **b** EM parameters, **c** the impedance matching and **d** the attenuation constant of 3-APFD

HC-8 and HMC-8 share the same geometry configuration but differ in atom configuration. HC-8, lacking the Mn-N4-C configuration, only achieves an *RLmin* of −36.58 dB at 1.51 mm and an EAB of 3.92 GHz at 1.7 mm. The permittivity and attenuation constant of HC-8 are significantly weaker than those of HMC-8 because of the absence of orbital coupling and spin polarization caused by the Mn-N4-C configuration. Thus, the EMW attenuation ability decreases dramatically, indicating that the internal atomic configuration is crucial in determining the EM properties of the material, even with the same geometry configuration.

Fig. S11 a 3D *RL* curve, **b** EM parameters, **c** the impedance matching and **d** the attenuation constant of HC-8

S2.11 FESEM of different graphite domain sizes

Fig. S12 FESEM images of **a** HMC-7 and **b** HMC-9

S2.12 Graphite domain sizes

Table S1 The graphite domain sizes, defects distance, and defect density

S2.13 Electromagnetic characteristic of different graphite domain sizes

Fig. S13 EM parameters and the impedance matching of **a-c** HMC-9, **b-d** HMC-7, respectively. **e** Attenuation constant of HMC-9 and HMC-7. **f** *MEAIA* of HMC-8 and HMC-7

S2.14 Electromagnetic simulations

Fig. S14 a The electric field distribution, **b** the magnetic field distribution, and **c** the power loss density of HMC-8, SHMC-8 and LHMC-8 at 2 GHz

Fig. S15 a The electric field distribution, **b** the magnetic field distribution, and **c** the power loss density of HMC-8, SHMC-8 and LHMC-8 at 12 GHz

Cross polarization was further verified by comparing the electric field loss strength and magnetic field loss strength of different structures. Two different models, the helical and spherical models, were simulated using the same electromagnetic parameters. As shown in **Figs. S16a-d**, the electric field and magnetic field loss strengths of the helical structure are approximately 4 and 1.7 times those of the spherical model, respectively. This is because the discontinuity of the boundary of the helical structure prevents the generated electromagnetic field components from offsetting each other. The stronger attenuation demonstrates that cross polarization is present, clearly showing that the geometric configuration plays a decisive role in electromagnetic loss under the same electromagnetic parameters.

Fig. S16 Electric field and magnetic field simulation of **a-b** helical structure and **c-d** sphere structure at 17.6 GHz

Fig. S17 Frequency dependence of variation of *RL* values and simulation thickness of **a** SMC-8, **b** SHMC-8, **c** HMC-8, **d** LHMC-8, **e** LMC-8, and **f** HMC-7

Fig. S18 Power loss density of the gradient metamaterial at **a** 6.9 GHz, **b** 10.8 GHz, and **c** 18 GHz

S2.17 RCS simulations

Fig. S19 a-f 3D RCS of HMC-7, HMC-8, HMC-9, SMC-8, LMC-8, and LHMC-8. **gj** The 2D RCS of HMC-9, LHMC-8, SMC-8, and LMC-8

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