

Supporting Information for

## 3D Ultralight Hollow NiCo Compound@MXene Composites for Tunable and High-efficient Microwave Absorption

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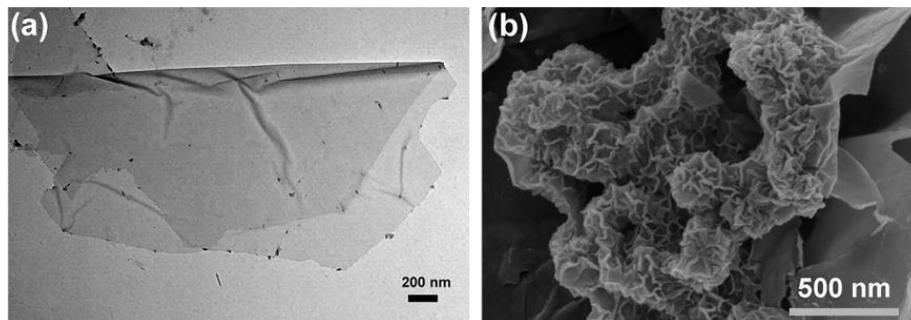
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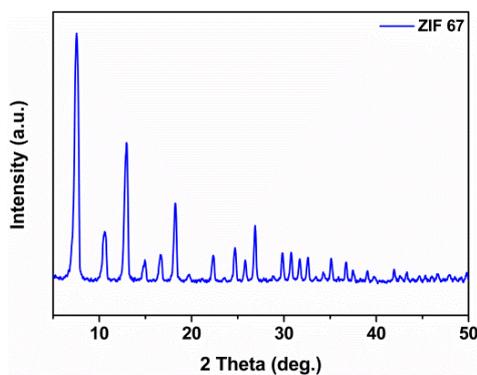
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### Supplementary Tables and Figures



**Fig. S1** **a** TEM images of  $\text{Ti}_3\text{C}_2\text{T}_x$  nanosheets. **b** SEM image of LDHT composites



**Fig. S2** XRD patterns of ZIF 67 precursor

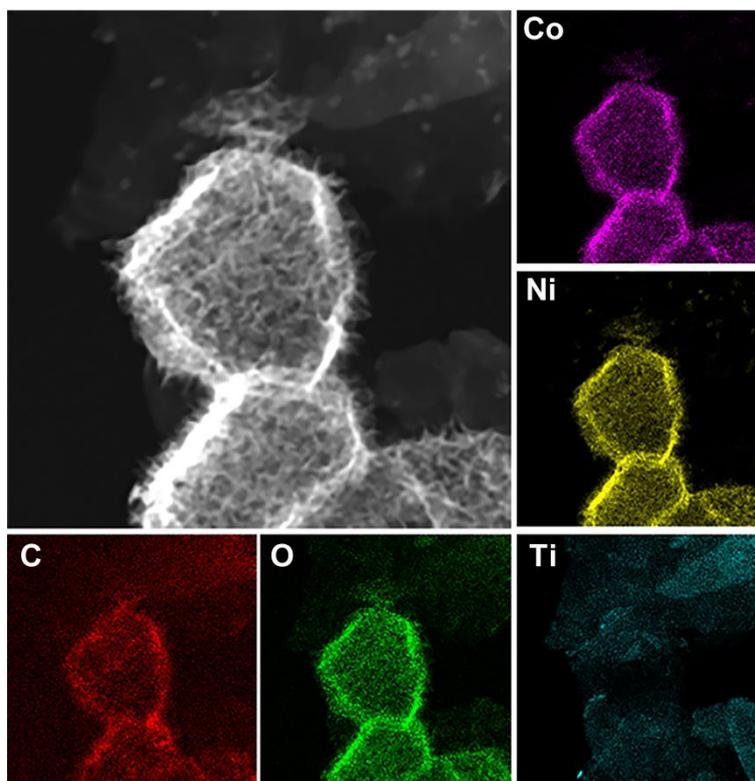


Fig. S3 Element mapping images of LDHT

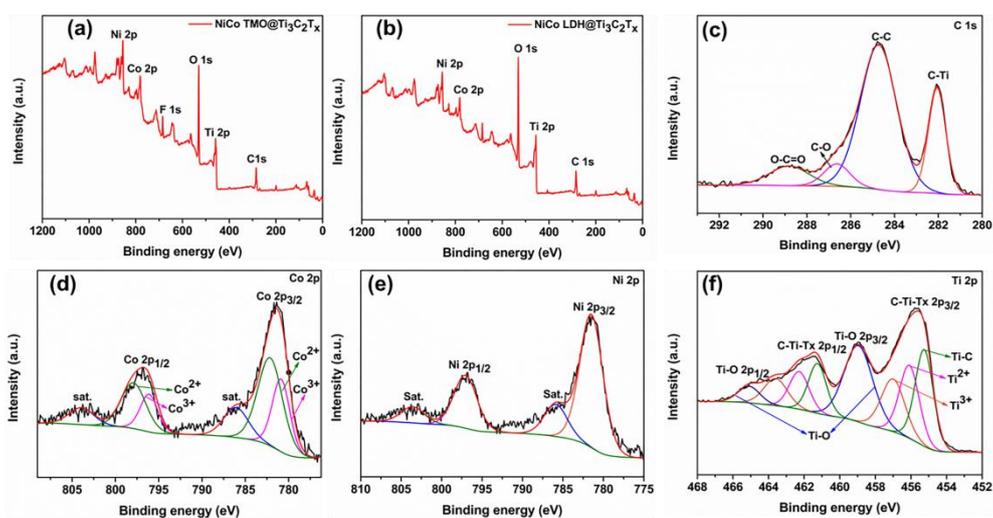
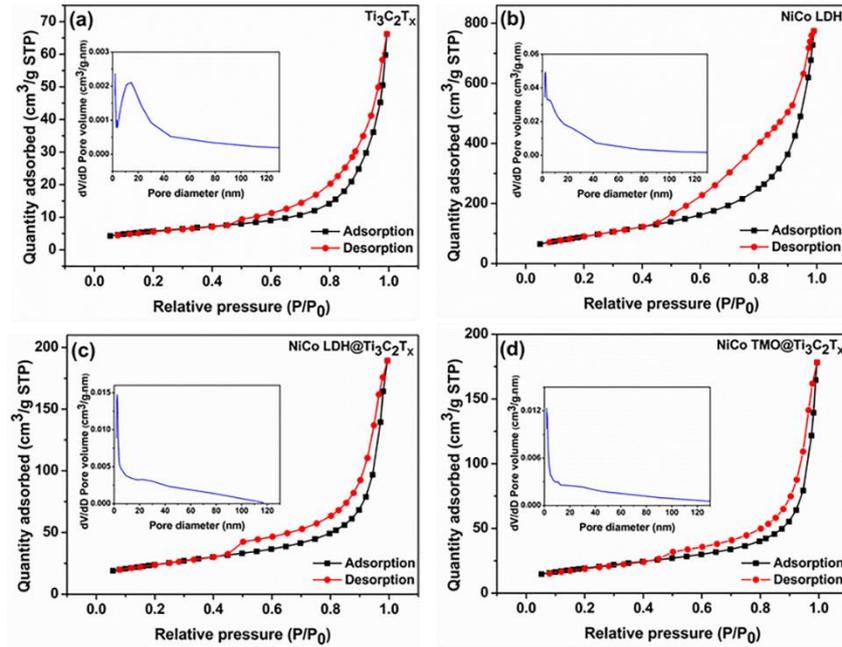


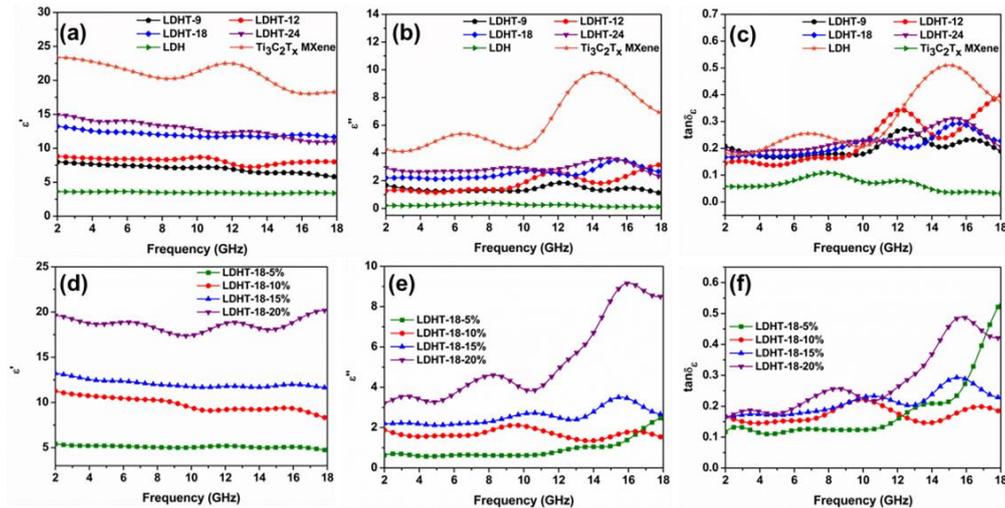
Fig. S4 a, b X-ray photoelectron spectroscopy (XPS) survey of TMOT and LDHT composites. c C 1s, d Co 2p, e Ni 2p, f Ti 2p XPS spectra of LDHT composites



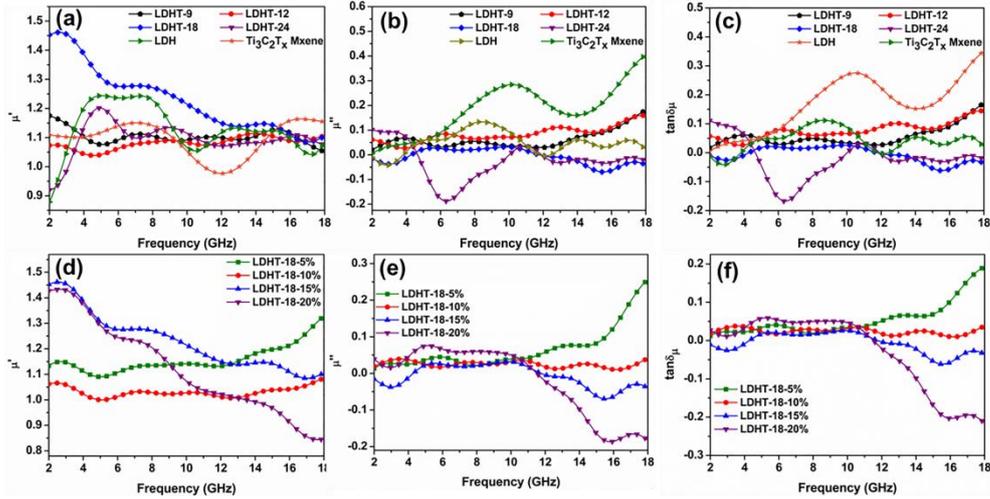
**Fig. S5** Nitrogen adsorption–desorption isotherms and the pore diameter distribution: **a** Ti<sub>3</sub>C<sub>2</sub>T<sub>x</sub>, **b** NiCo LDH, **c** LDHT and **d** TMOT composites



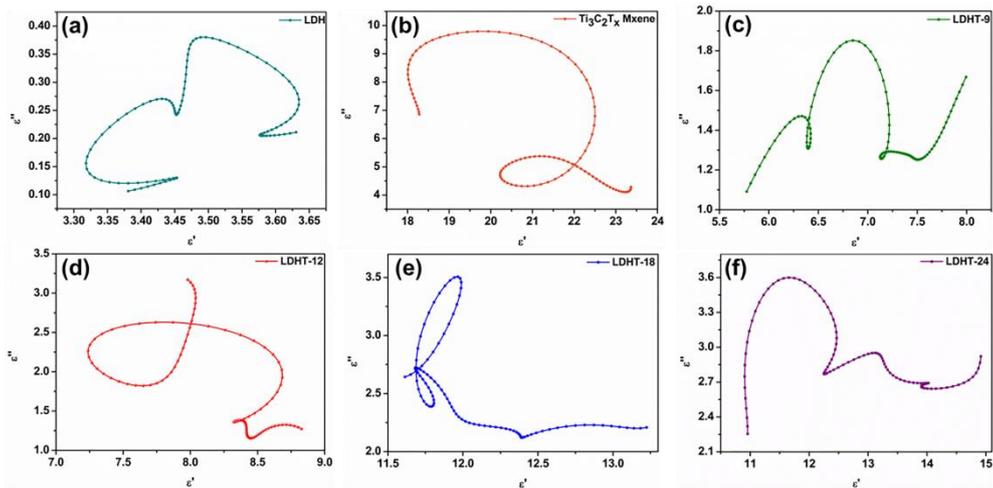
**Fig. S6** Images of LDHT flexible film absorbers



**Fig. S7** Frequency dependence of complex permittivity for various composites: **a** Real part  $\epsilon'$ , **b** imaginary part  $\epsilon''$ , **c** dielectric loss tangent of Ti<sub>3</sub>C<sub>2</sub>T<sub>x</sub>, LDH and LDHT-x composites with filler content of 15 wt%. **d** Real part  $\epsilon'$ , **e** imaginary part  $\epsilon''$ , **f** dielectric loss tangent of LDHT-18 composites at different loadings



**Fig. S8** **a** Real part  $\mu'$ , **b** imaginary part  $\mu''$ , **c** magnetic loss tangent of complex permeability for  $\text{Ti}_3\text{C}_2\text{T}_x$ , LDH and LDHT- $x$  composites with filler content of 15 wt% **d** real part  $\mu'$ , **e** imaginary part  $\mu''$ , **f** magnetic loss tangent of complex permeability for LDHT-18 composites at different loadings



**Fig. S9** Relationship between real and imaginary dielectric part of various samples: **a** LDH, **b**  $\text{Ti}_3\text{C}_2\text{T}_x$ , **c** LDHT-9, **d** LDHT-12, **e** LDHT-18, **f** LDHT-24

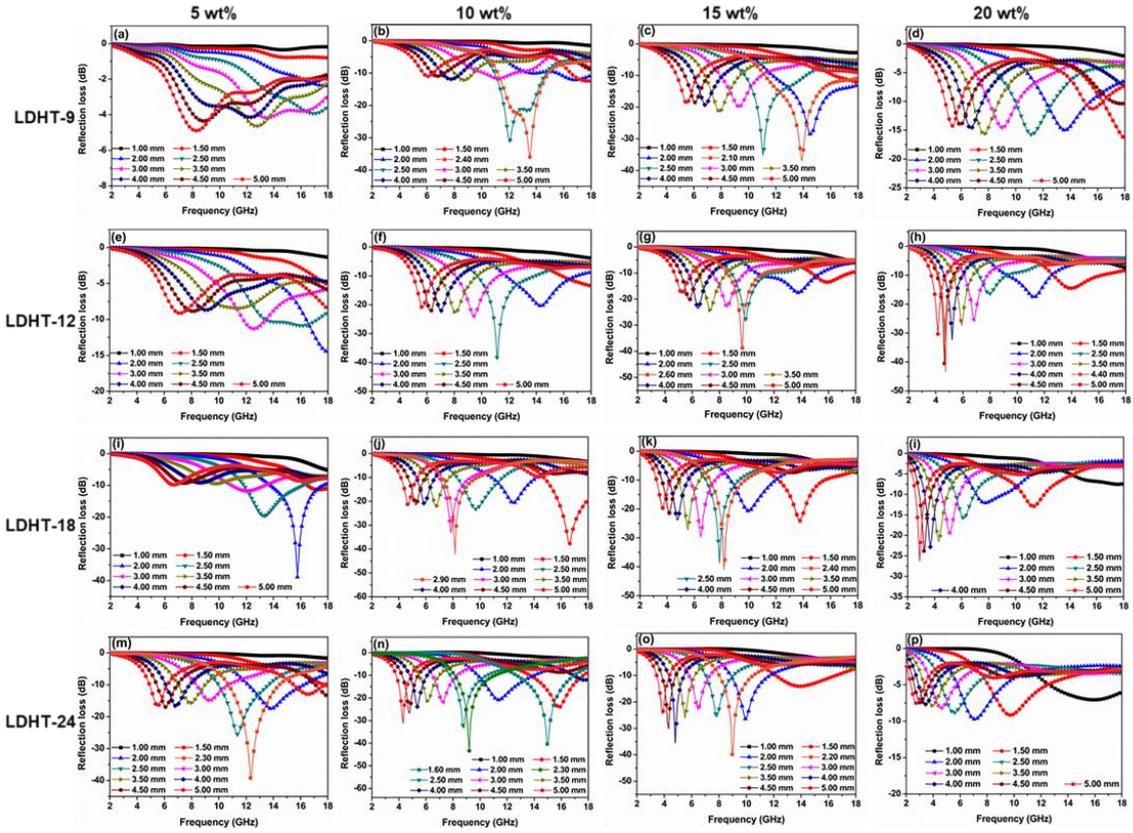


Fig. S10 2D RL curves of the LDHT-x series

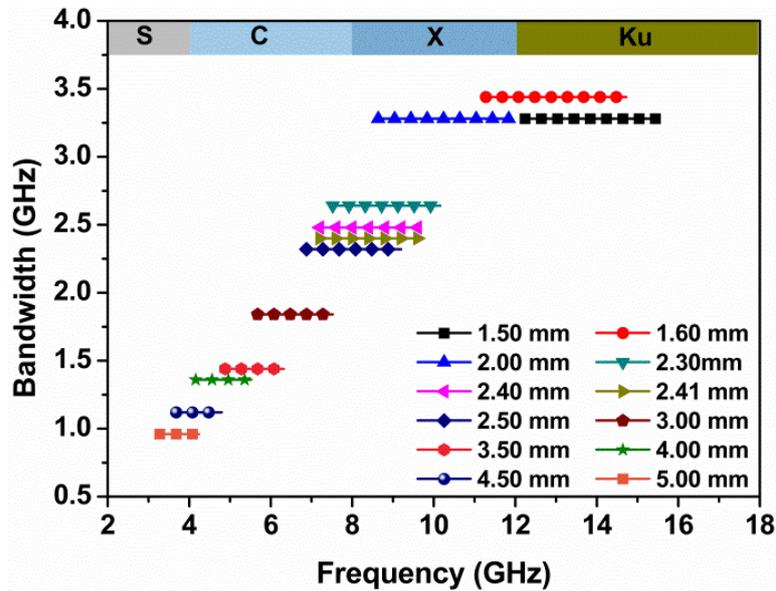


Fig. S11 Effective absorbing bandwidth of LDHT-18 at different thicknesses composites with 15 wt% filler content

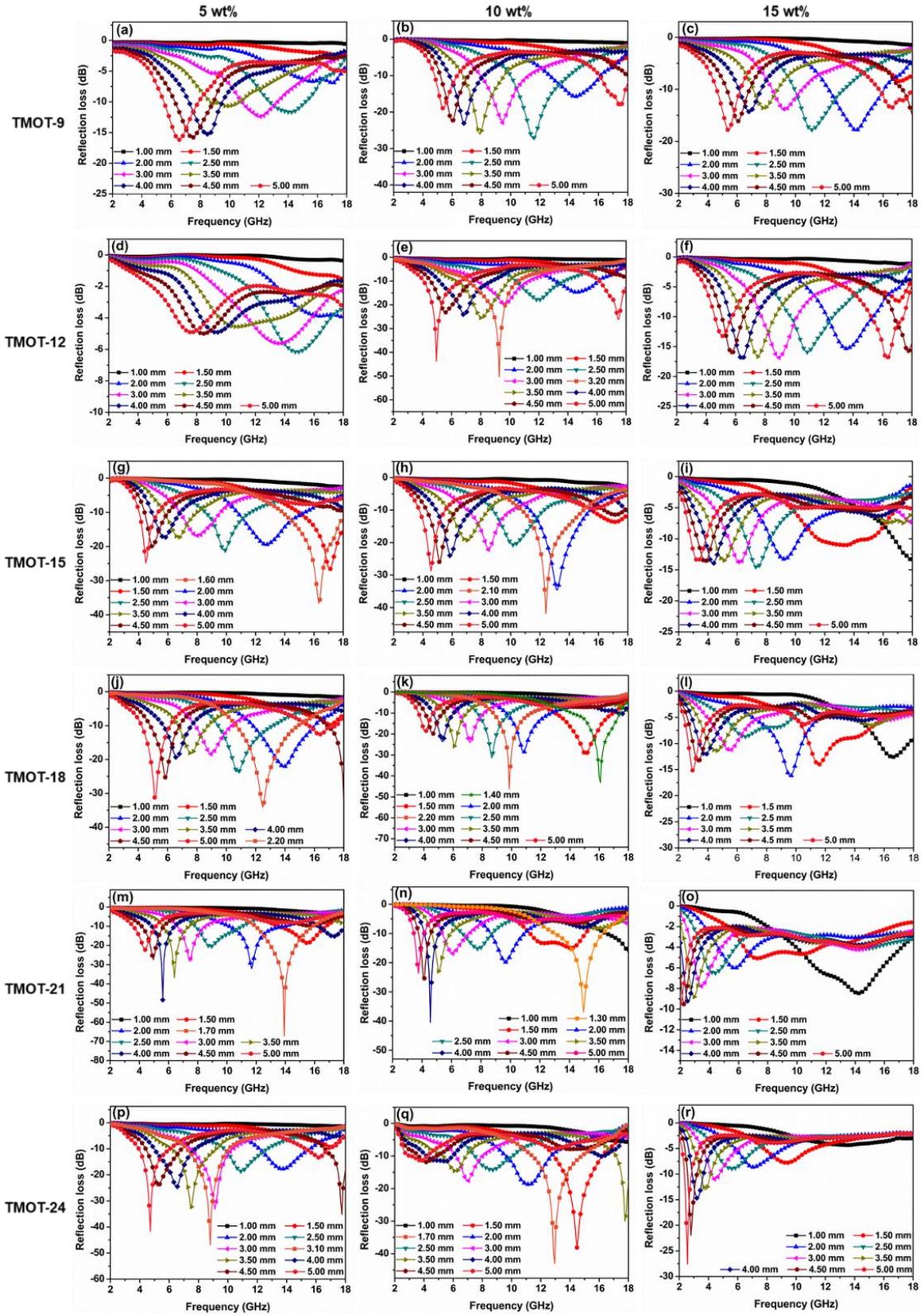
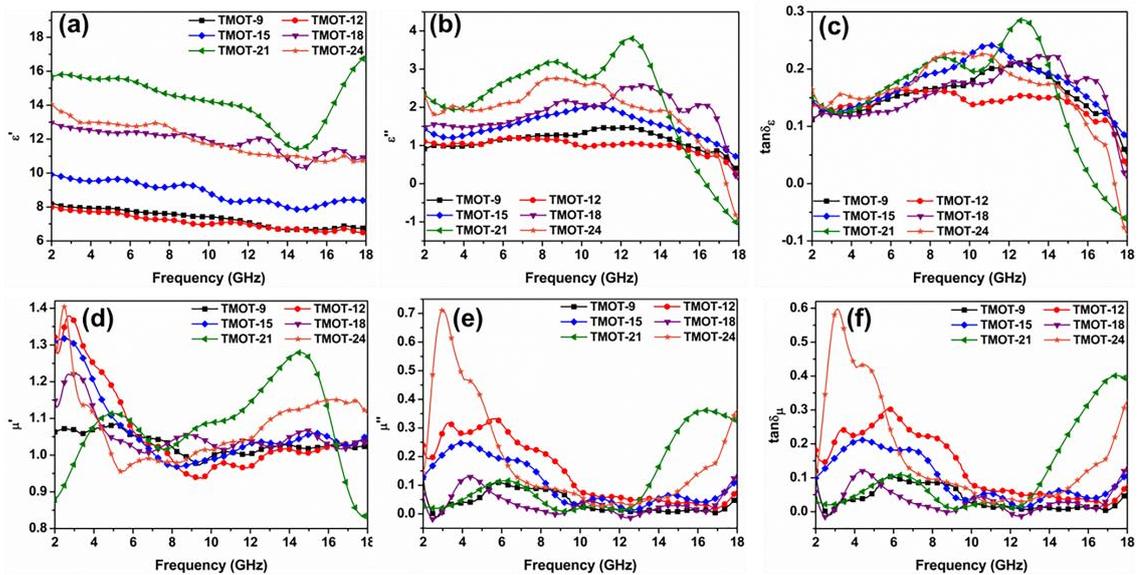


Fig. S12 2D RL curves of the TMOT-x series

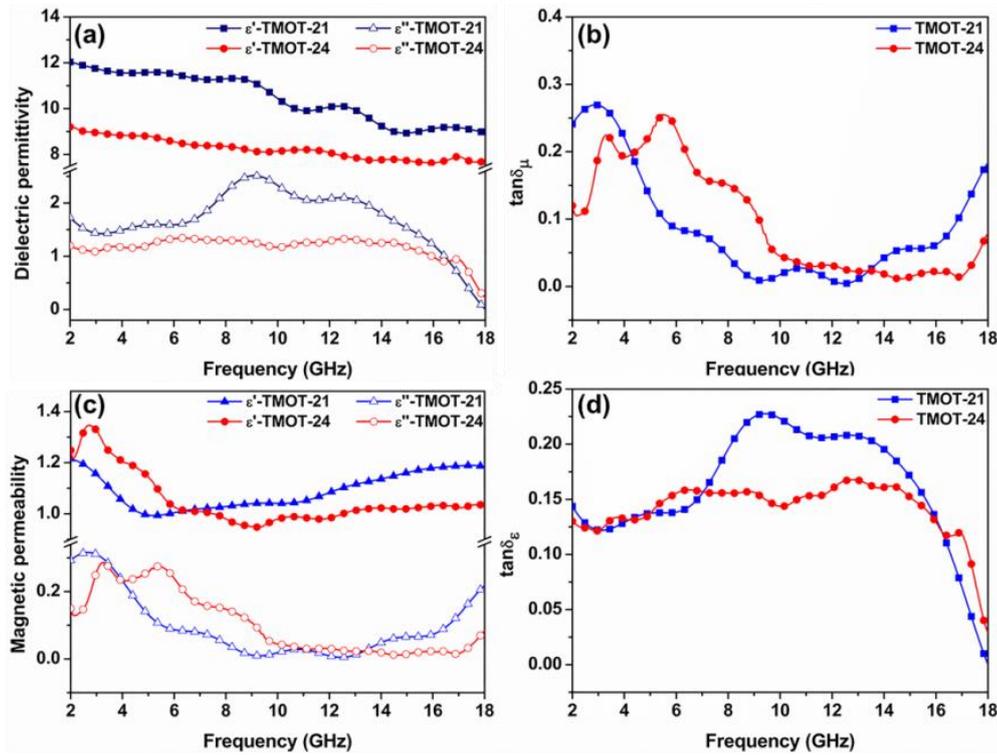
Overall, the  $\epsilon'$  values of all TMOT-x samples exhibit a downward trend with the increasing frequency revealing a typical frequency dispersion phenomenon and are intimately determined to the load of  $\text{Ti}_3\text{C}_2\text{T}_x$  (Fig. S13). With raised  $\text{Ti}_3\text{C}_2\text{T}_x$  decoration, the  $\epsilon'$  and  $\epsilon''$  values first increased and then decreased, which is attributed to increase in current leakage engendered from the increased area of MXene nanosheets contact [S1, S2]. By contrast, the dielectric properties of TMOT-x samples are enhanced than those of LDHT-x composites, mainly due to the large number oxygen vacancies which act as polarization center and are beneficial to electromagnetic wave absorption. During the calcination process, part of the  $\text{Co}^{3+}$  is reduced to  $\text{Co}^{2+}$  as proved in XPS spectra, resulting in disordered lattice arrangement and formation of oxygen vacancies. Interestingly, the presence of oxygen vacancies will bind the surrounding electrons and act as electron donors, facilitating charge transfer and separation to generate polarization center [S3]. As illustrated in Fig. S13d-f, the values of  $\mu'$  and  $\mu''$  for all TMOT-x composites basically hold similar change trends and suddenly decrease over 2.0–7.0 GHz and then fluctuate in a gentle way, indicating that the magnetic loss also make a relevant contribution to microwave absorption. As represented in Fig. S13 c,f, it is no surprise that the variation trends of  $\tan\delta_\epsilon$  and  $\tan\delta_\mu$  are similar with these of  $\epsilon'$  and  $\mu''$ .



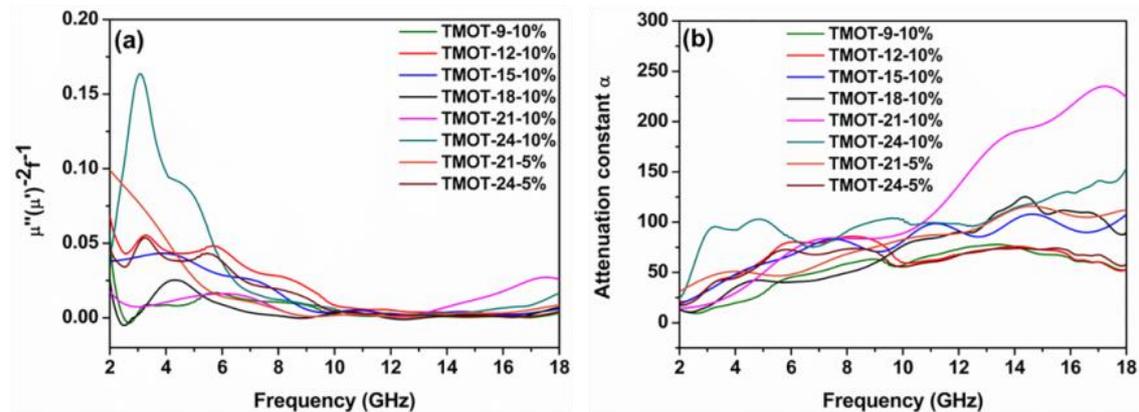
**Fig. S13** **a** Real part  $\epsilon'$ , **b** imaginary part  $\epsilon''$ , **c** dielectric loss tangent of complex permittivity, **d** real part  $\mu'$ , **e** imaginary part  $\mu''$ , **f** magnetic loss tangent of complex permeability of TMOT-x composite with the filler loading of 10 wt%

Generally, the magnetic loss mainly comes from natural resonance, exchange resonance and eddy current loss in 2-18 GHz, whereas the domain wall resonance usually generated in the 1–100 MHz and the hysteresis loss in this weak magnetic field can be neglected. Universally, the eddy current loss can be evaluated by the values of the eddy current coefficient  $C_0(C_0=\mu''(\mu')^{-2}f^{-1})$  and shown in Fig. S15. If  $C_0$  is a constant as the frequency changes, the eddy current loss should be the individual loss mechanism. However, it is clear that TMOT-x appears intensive fluctuations in the range of 2-10 GHz, elucidating that both the eddy current loss and natural resonance loss contributes

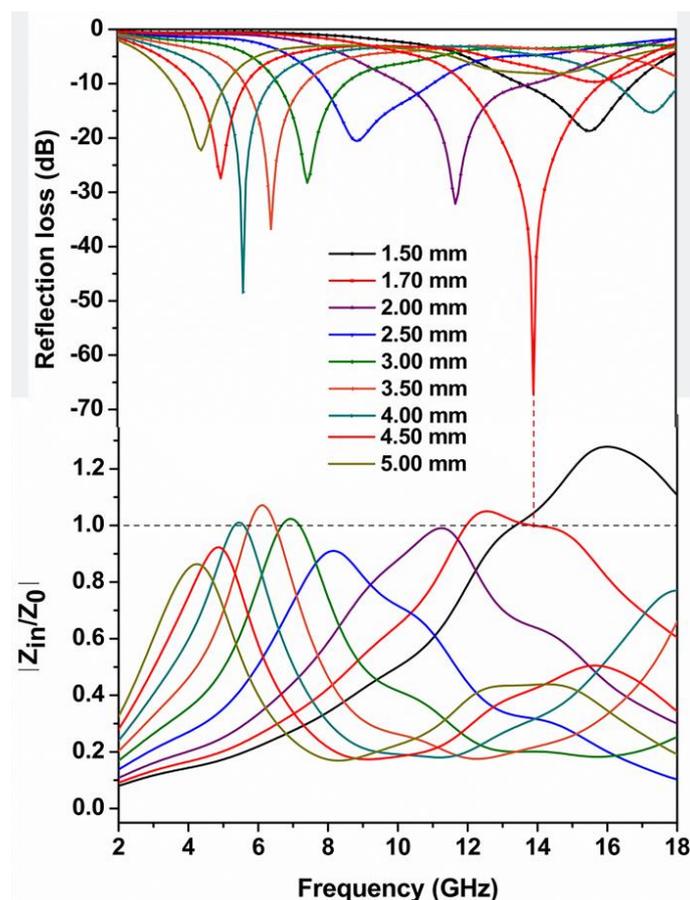
to the magnetic loss. The values of attenuation constant increase linearly with the increase of frequency, and improve slightly with the increase of  $Ti_3C_2T_x$  adherent, excluding TMOT-24-10%. Besides, the  $\alpha$  values of TMOT-x samples also enhance compared with LDHT-x composites at the same filler loading, which is beneficial to optimize microwave absorption property. For TMOT-21 composites with 5 wt% filler loading, the impedance matching effect occurs optimally at a thickness of 1.70 mm, meanwhile the  $RL_{min}$  predictably exceeded -67.22 GHz as shown in Fig. S16.



**Fig. S14** Electromagnetic parameters of TMOT-21 and TMOT-24 composites with the filler loading of 5 wt%: **a** complex permittivity, **b** dielectric loss tangent, **c** complex permeability and **d** magnetic loss tangent of TMOT-x composites



**Fig. S15 a** Calculated  $\mu''(\mu')^{-2}f^{-1}$ , **b**  $\alpha$  value of series TMOT composites over the entire frequency of 2-18 GHz



**Fig. S16** Frequency dependence of RL and the relative input impedance ( $|Z_{in}/Z_0|$ ) curves of TMOT-21 with 5 wt% filler loading

### Supplementary References

- [S1] Z. Wang, Z. Cheng, C.Q. Fang, X.L. Hou, L. Xie, Recent advances in MXenes composites for electromagnetic interference shielding and microwave absorption. *Compos. Part A Appl. Sci. Manuf.* **136**, 105956 (2020). <https://doi.org/10.1016/j.compositesa.2020.105956>
- [S2] M.S. Cao, Y.Z. Cai, P. He, J.C. Shu, W.Q. Cao et al., 2D MXenes: Electromagnetic property for microwave absorption and electromagnetic interference shielding. *Chem. Eng. J.* **359**, 1265-1302 (2019). <https://doi.org/10.1016/j.cej.2018.11.051>
- [S3] T.Q. Hou, B.B. Wang, M.L. Ma, A.L. Feng, Z.Y. Huang et al., Preparation of two-dimensional titanium carbide ( $Ti_3C_2T_x$ ) and  $NiCo_2O_4$  composites to achieve excellent microwave absorption properties. *Compos. Part B Eng.* **180**, 107577 (2020). <https://doi.org/10.1016/j.compositesb.2019.107577>